

Extremum Seeking Control for Antenna Pointing via Symmetric Product Approximation*

Bo Wang * Hashem Ashrafiou ** Sergey G. Nersesov **

* Department of Mechanical Engineering, The City College of New York, New York, NY 10031, USA (e-mail: bwang1@ccny.cuny.edu).

** Department of Mechanical Engineering, Villanova University, Villanova, PA 19085, USA (e-mail: {hashem.ashrafiou, sergey.nersesov}@villanova.edu)

Abstract: This paper investigates extremum seeking control for a torque-controlled antenna pointing system without direct angular measurements. We consider a two-degree-of-freedom (2-DOF) antenna system that receives an unknown signal from its environment, where the signal strength varies with the antenna's orientation. It is assumed that only real-time measurements of the signal are available. We develop an extremum seeking control strategy that enables the antenna to autonomously adjust its direction to maximize the received signal strength based on the symmetric product approximation. Under suitable assumptions on the signal function, we prove local practical uniform asymptotic stability for the closed-loop system.

Copyright © 2025 The Authors. This is an open access article under the CC BY-NC-ND license (<https://creativecommons.org/licenses/by-nc-nd/4.0/>)

Keywords: Extremum seeking, antenna pointing, averaging, symmetric product approximation.

1. INTRODUCTION

Satellite communication is one of the fastest-growing fields in science and technology, enabling global information exchange. Antennas play a crucial role in signal transmission and reception, with the quality of the received signal depending on the satellite's relative position and the antenna's orientation. However, manual adjustments to the antenna's orientation are often impractical, particularly when antennas are mounted on mobile vehicles or used in large-scale systems. Therefore, to ensure the strongest, best-quality signal reception, automatic antenna pointing control systems are essential for accurately aligning antennas with the signal source (Mulla and Vasambekar, 2016).

Traditional antenna pointing control strategies, such as PI, LQG, and H_∞ , often assume that the reference attitude of the antenna is known, and the difference between the reference and the antenna attitude as sensed by encoders (Gawronski, 2001, 2007). In many practical scenarios, it is reasonable to assume that the antenna attitude is measurable by encoders. However, the reference (desired) attitude of the antenna is usually *unknown*, which is typically determined by the signal source. In general, the desired antenna direction is the one that maximizes the received signal strength. In such cases, traditional antenna pointing control algorithms may not be applied.

Extremum seeking is a real-time model-free optimization approach that is applicable to dynamical systems (Ariyur and Krstić, 2003; Scheinker and Krstić, 2017). The interest in extremum seeking algorithms is greatly motivated by

various real-world problems, which require optimizing the performance of dynamic systems based on measurable but analytically unknown functions. Applications include localization of sources for autonomous vehicles (Suttner, 2019; Wang et al., 2023), maximum power point tracking, and bioreactor growth rate optimization, etc. We refer the reader to Scheinker (2024) for an interesting survey.

According to different types of averaging techniques, extremum seeking schemes can be categorized into classical averaging-based (Ariyur and Krstić, 2003), Lie bracket averaging-based (Dürr et al., 2013, 2017), and symmetric product approximation-based seekers (Suttner, 2022; Suttner and Krstić, 2023). The classical averaging-based approach and the Lie bracket averaging-based approach work well for first-order kinematic systems; however, their extension to second-order mechanical systems is limited. The symmetric product approximation-based approach, which is based on the averaging results in Bullo (2002) for mechanical systems under vibrational control, is applicable to a much larger class of (kinematic-kinetic) mechanical systems. Applications of this strategy to autonomous vehicles can be found in Suttner (2019); Wang et al. (2023).

Applying extremum seeking strategies to antenna pointing systems is intriguing because, as mentioned earlier, the desired antenna attitude is determined by an analytically unknown signal function and is typically unknown. Extremum seeking methods offer an alternative approach to adjusting the antenna's orientation to maximize the received signal strength. In Shore et al. (2024), three classical averaging-based extremum seeking methods for antenna pointing are compared under different simulation scenarios. The methods proposed in Shore et al. (2024) rely on

* This work was supported in part by GSoE at CCNY, and in part by the PSC-CUNY Award, jointly funded by The Professional Staff Congress and The City University of New York.

the Taylor series approximation of the objective function, however, no stability analysis or results are provided.

In this paper, we study the problem of extremum seeking control for a torque-controlled antenna pointing system. We consider a two-degree-of-freedom (2-DOF) antenna system that receives an unknown signal from its environment, where the signal strength varies with the antenna's orientation. Only real-time signal measurements are assumed to be available. We develop an extremum seeking control strategy based on the symmetric product approximation, enabling the antenna to autonomously adjust its direction to maximize the received signal strength. The contributions of this paper can be summarized as follows: (i) From the theoretical viewpoint, we provide a stability proof for the closed-loop system. Specifically, we show that under suitable assumptions on the signal function, the origin of the closed-loop system is locally practically uniformly asymptotically stable. (ii) From the practical viewpoint, the proposed seeking scheme does not require posture measurements, relying only on real-time signal measurements. Its structure is exceptionally simple and easy to implement—the measured signal is multiplied by periodic signals and fed into the torque input. To the best of the authors' knowledge, this marks the first application of the symmetric product approximation-based extremum seeking approach to antenna pointing systems.

2. PROBLEM STATEMENT AND PRELIMINARIES

Notation: Let $|\cdot|$ denote the Euclidean norm on \mathbb{R}^n . For real matrices A , we use the matrix norm $\|A\| := \sup\{|Ax| : |x| = 1\}$, and $I_{n \times n} \in \mathbb{R}^{n \times n}$ the identity matrix. Recall that for any real matrix $A := [a_{ij}] \in \mathbb{R}^{n \times p}$, $\|A\| \leq \sqrt{np} \max_{i,j} |a_{ij}|$. We use the notations $s_\theta := \sin(\theta)$ and $c_\theta := \cos(\theta)$ for simplicity. Throughout this article, we omit the arguments of functions when they are clear from the context.

2.1 Modeling of the Antenna Pointing System

Consider a simplified 2-DOF antenna system shown in Fig 1. It is modeled as a rectangular cuboid supported by a frame with respect to which the antenna rotates by the angle θ_1 . This frame in turn is attached to the disk that rotates about the vertical axis by the angle θ_2 . Both rotations are actuated by two independent motors whose torques are control variables τ_1 and τ_2 , respectively. Two reference frames are introduced to describe the motion of the antenna: the stationary reference frame \mathcal{I} , with unit vectors \vec{I} , \vec{J} , and \vec{K} , and the body-fixed reference frame \mathcal{A} , whose coordinate system, with unit vectors \vec{i} , \vec{j} , and \vec{k} , is fixed at the mass center of the antenna. Since the antenna is modeled as a rectangular cuboid, axes passing through its mass center that are parallel to the unit vectors \vec{i} , \vec{j} , \vec{k} are principal axes of inertia. In the principal axes of inertia, the equations of rotational motion for the antenna are given by

$$M_x = I_x \dot{\omega}_x - (I_y - I_z) \omega_y \omega_z, \quad (1a)$$

$$M_y = I_y \dot{\omega}_y - (I_z - I_x) \omega_z \omega_x, \quad (1b)$$

$$M_z = I_z \dot{\omega}_z - (I_x - I_y) \omega_x \omega_y, \quad (1c)$$

where I_x , I_y , I_z are antenna's principal moments of inertia; ω_x , ω_y , ω_z are components (in projection onto \mathcal{A}) of the

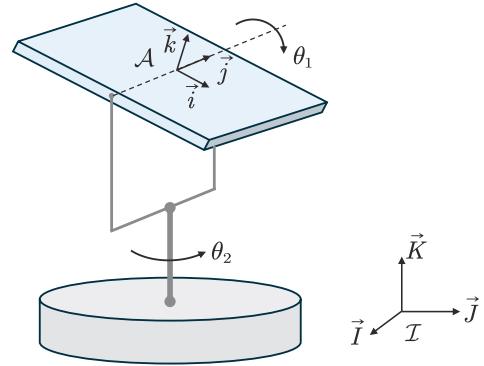


Fig. 1. Schematic diagram of the antenna pointing system. antenna's angular velocity vector $\vec{\omega}_{\mathcal{A}/\mathcal{I}}$ with respect to \mathcal{I} , i.e., $\vec{\omega}_{\mathcal{A}/\mathcal{I}} = \omega_x \vec{i} + \omega_y \vec{j} + \omega_z \vec{k}$. The terms M_x , M_y , M_z are components (in projection onto \mathcal{A}) of the total external moment \vec{M} acting on the antenna with respect to its mass center, i.e., $\vec{M} = M_x \vec{i} + M_y \vec{j} + M_z \vec{k}$.

Next, we relate the angular rates ω_x , ω_y , ω_z with the angles θ_1 and θ_2 . Note that $\vec{\omega}_{\mathcal{A}/\mathcal{I}} = \dot{\theta}_1 \vec{j} + \dot{\theta}_2 \vec{K}$ and $\vec{K} = -\sin \theta_1 \vec{i} + \cos \theta_1 \vec{k}$. Thus,

$$\vec{\omega}_{\mathcal{A}/\mathcal{I}} = -\dot{\theta}_2 \sin \theta_1 \vec{i} + \dot{\theta}_1 \vec{j} + \dot{\theta}_2 \cos \theta_1 \vec{k},$$

which implies that

$$\omega_x = -\dot{\theta}_2 \sin \theta_1, \quad \omega_y = \dot{\theta}_1, \quad \omega_z = \dot{\theta}_2 \cos \theta_1. \quad (2)$$

The total external moment \vec{M} acting on the antenna consists of two torques rotating it about \vec{j} and \vec{K} axes and corresponding rotational damping moments along those axes, i.e., $\vec{M} = (\tau_1 - d_1 \dot{\theta}_1) \vec{j} + (\tau_2 - d_2 \dot{\theta}_2) \vec{K}$, where $d_1 > 0$ and $d_2 > 0$ are rotational damping coefficients. Substituting $\vec{K} = -\sin \theta_1 \vec{i} + \cos \theta_1 \vec{k}$ into \vec{M} yields

$$M_x = -\tau_2 \sin \theta_1 + d_2 \dot{\theta}_2 \sin \theta_1, \quad (3a)$$

$$M_y = \tau_1 - d_1 \dot{\theta}_1, \quad (3b)$$

$$M_z = \tau_2 \cos \theta_1 - d_2 \dot{\theta}_2 \cos \theta_1. \quad (3c)$$

Here τ_1 and τ_2 are control variables.

Consequently, the model of the antenna pointing system can be in the following Euler-Lagrangian form

$$\dot{\theta} = J(\theta)\omega \quad (4a)$$

$$I\dot{\omega} + C(\omega)\omega + D\omega = J(\theta)^\top \tau \quad (4b)$$

where $\theta := [\theta_1 \ \theta_2]^\top$, $\omega := [\omega_x \ \omega_y \ \omega_z]^\top$, $\tau := [\tau_1 \ \tau_2]^\top$, $I := \text{diag}\{I_x, I_y, I_z\} > 0$, $D := \text{diag}\{d_2, d_1, d_2\} > 0$, and

$$J(\theta) := \begin{bmatrix} 0 & 1 & 0 \\ -s_{\theta_1} & 0 & c_{\theta_1} \end{bmatrix}, \quad C(\omega) := \begin{bmatrix} 0 & I_z \omega_z & -I_y \omega_y \\ -I_z \omega_z & 0 & I_x \omega_x \\ I_y \omega_y & -I_x \omega_x & 0 \end{bmatrix}.$$

2.2 Problem Statement

We assume that the antenna receives an analytically unknown signal from its environment, and the received power p is measurable in real-time. The objective is to design a feedback control law τ to adjust the antenna's orientation θ to maximize the received power $p(\theta(t))$, i.e., to solve the maximization problem $\max_{\tau} p(\theta)$ in real-time. However, to maintain consistency with the extremum-seeking

literature and without loss of generality, we consider the equivalent minimization problem, *i.e.*, $\min_{\theta} h(\theta)$, where $h(\theta) := -p(\theta) + p_0$ and p_0 can be an arbitrary real number. We make the following assumptions on the objective function h .

Assumption 1. Assume that the angle-dependent nonlinear cost function $h(\theta)$ is smooth, positive everywhere, and has a global minimum point. That is, there exists a unique $\theta_* := [\theta_{1*} \ \theta_{2*}]^\top$ such that

$$\frac{\partial h}{\partial \theta}(\theta_*) = 0, \quad \text{and} \quad \frac{\partial^2 h}{\partial \theta^2}(\theta) \neq 0, \quad \forall \theta \neq \theta_*. \quad (5)$$

Assumption 2. The cost function h is in the separable form

$$h(\theta) = h_1(\theta_1) + h_2(\theta_2). \quad (6)$$

Assumption 3. The Hessian matrix of the cost function is globally bounded. That is, there exists $h_M > 0$ such that

$$\left\| \frac{\partial^2 h}{\partial \theta^2}(\theta) \right\| \leq h_M, \quad \forall \theta. \quad (7)$$

The antenna can measure the value of $h(\theta(t))$ in real-time. Note that both the extremum θ_* and the gradient $\frac{\partial h}{\partial \theta}(\theta)$ are unknown.

Remark 1. Assumption 1 is a regular assumption in the extremum-seeking literature. Assumptions 2 and 3 are technical assumptions. Specifically, Assumption 2 shows that the partial derivatives of h in each direction are independent. One should notice that the objective function used in Shore et al. (2024) satisfies Assumptions 1-3. In fact, modeling the received power as a Gaussian function of the pointing error yields a quadratic objective function that satisfies Assumptions 1-3.

2.3 Practical Stability

We use the same stability notion as in Moreau and Aeyels (2000); Dürr et al. (2013). Consider the time-varying system that depends on a parameter $\varepsilon \in (0, \varepsilon_0]$

$$\dot{x} = f^\varepsilon(t, x), \quad x \in \mathbb{R}^n, \quad (8)$$

where $\varepsilon_0 > 0$. We assume that for each ε , the function f^ε is continuous, and $f^\varepsilon(t, \cdot)$ is locally Lipschitz uniformly in t . For every $\varepsilon \in (0, \varepsilon_0]$ and every $t \in \mathbb{R}$, let $\phi_t^\varepsilon : \mathbb{R}^n \rightarrow \mathbb{R}^n$ be a diffeomorphism. Denote the new variable as $\tilde{x} := \phi_t^\varepsilon(x)$.

Definition 1. (Dürr et al. (2013)). Let $x_* \in \mathbb{R}^n$ and let S be a neighborhood of x_* in \mathbb{R}^n . We say that x_* is *S-practically uniformly asymptotically stable* for (8) in the variable $\tilde{x} := \phi_t^\varepsilon(x)$ if the following two conditions are both satisfied:

(i) *Practical Uniform Stability.* For every $c_1 > 0$, there exist c_2 and $\varepsilon_0 > 0$ such that for all $\varepsilon \in (0, \varepsilon_0]$ and all $t_0 \in \mathbb{R}$

$$|\tilde{x}_0 - x_*| \leq c_2 \implies |\tilde{x}(t) - x_*| \leq c_1, \quad \forall t \geq t_0,$$

where $\tilde{x}(t) := \phi_t^\varepsilon(x(t))$ and $x(t)$ represents the solution of (8) with initial condition $x(t_0) = (\phi_{t_0}^\varepsilon)^{-1}(\tilde{x}_0)$.

(ii) *S-Practical Uniform Attractivity.* For all $c_1, c_2 > 0$, there exist T, R , and $\varepsilon_0 > 0$ such that for all $\varepsilon \in (0, \varepsilon_0]$, all $t_0 \in \mathbb{R}$, and all $\tilde{x}_0 \in S$ with $|\tilde{x}_0 - x_*| \leq c_1$

$$|\tilde{x}(t) - x_*| \leq R, \quad \forall t \geq t_0,$$

$$|\tilde{x}(t) - x_*| \leq c_2, \quad \forall t \geq t_0 + T,$$

where $\tilde{x}(t) := \phi_t^\varepsilon(x(t))$ and $x(t)$ represents the solution of (8) with initial condition $x(t_0) = (\phi_{t_0}^\varepsilon)^{-1}(\tilde{x}_0)$.

If the conditions in Definition 1 are satisfied for an unknown, arbitrarily small neighborhood S of x_* in \mathbb{R}^n , then we say that x_* is *locally* practically uniformly asymptotically stable for (8) in the variable \tilde{x} . If there exists a vector field \bar{f} such that $f^\varepsilon = \bar{f}$ for all $\varepsilon \in (0, \varepsilon_0]$, then we omit the word “practical” in Definition 1.

Next, let us consider the time-varying system

$$\dot{x} = \bar{f}(t, \bar{x}), \quad \bar{x} \in \mathbb{R}^n, \quad (9)$$

where \bar{f} is locally Lipschitz in x uniformly in t .

Definition 2. (Converging Trajectories Property). We say that *the solutions of (8) in the variable $\tilde{x} := \phi_t^\varepsilon(x)$ approximate the solutions of (9)*, if for every $T, d > 0$ and every compact set $K \subset \mathbb{R}^n$, there exists $\varepsilon_0 > 0$ such that for all $t_0 \in \mathbb{R}$, and all $\tilde{x}_0 \in K$, the following implication holds: If the solution of (9) with initial condition $\bar{x}(t_0) = \tilde{x}_0$ satisfies $\bar{x}(t) \in K$ for every $t \in [t_0, t_0 + T]$, then for all $\varepsilon \in (0, \varepsilon_0]$, we have $|\tilde{x}(t) - \bar{x}(t)| \leq d$, $\forall t \in [t_0, t_0 + T]$, where $\tilde{x}(t) := \phi_t^\varepsilon(x(t))$ and $x(t)$ represents the solution of (8) with initial condition $x(t_0) = (\phi_{t_0}^\varepsilon)^{-1}(\tilde{x}_0)$.

Proposition 1. (Suttnar and Krstić (2023)). Let $x_* \in \mathbb{R}^n$ and let S be a neighborhood of x_* in \mathbb{R}^n . Assume that the solutions of (8) in the variable $\tilde{x} := \phi_t^\varepsilon(x)$ approximate the solutions of (9). If x_* is *S-uniformly asymptotically stable* for (9), then x_* is *S-practically uniformly asymptotically stable* for (8) in the variable \tilde{x} .

3. MAIN RESULTS

3.1 Control Law

Now we introduce the component of the control law. Let T be a positive real number. Let $u_1, u_2 : \mathbb{R} \rightarrow \mathbb{R}$ be two T -periodic, zero-mean, independent perturbation signals, where the zero-mean antiderivatives U_1 and U_2 of u_1 and u_2 satisfy the orthogonality condition

$$\int_0^T U_i(\tau) U_j(\tau) d\tau = \begin{cases} \frac{T}{2} & \text{if } i = j, \\ 0 & \text{if } i \neq j \end{cases} \quad (10)$$

for $i, j \in \{1, 2\}$. For instance, we can choose u_1 and u_2 as $\cos(qt)$ and $\sin(qt)$ for any $q \neq 0$. The proposed extremum seeking control law is given by

$$\tau_1 = \frac{k_1}{\varepsilon} u_1 \left(\frac{t}{\varepsilon} \right) h(\theta), \quad (11a)$$

$$\tau_2 = \frac{k_2}{\varepsilon} u_2 \left(\frac{t}{\varepsilon} \right) h(\theta), \quad (11b)$$

where ε , k_1 , and k_2 are positive control parameters. With the control law (11) we obtain the closed-loop system

$$\dot{\theta} = J(\theta) \omega \quad (12a)$$

$$I\dot{\omega} + C(\omega)\omega + D\omega = J(\theta)^\top \left[\frac{h(\theta)}{\varepsilon} K u \left(\frac{t}{\varepsilon} \right) \right], \quad (12b)$$

where $u(\cdot) := [u_1(\cdot) \ u_2(\cdot)]^\top$ and $K := \text{diag}\{k_1, k_2\}$. Next, our averaging analysis will show that the term in the bracket of (12b) approximates the negative gradient of the function $\frac{1}{4}h^2$.

3.2 Averaging Analysis

Our goal is to derive the averaged system from the closed-loop system (12) using the symmetric product approxi-

mation. Here, we recall the approach proposed in Bullo (2002); Bullo and Lewis (2005) and represent the results *in coordinates*. Let us rewrite the closed-loop system (12b) in the control-affine form

$$\dot{\omega} = Y_0(\omega) + \sum_{i=1}^2 \frac{1}{\varepsilon} u_i \left(\frac{t}{\varepsilon} \right) Y_i(\theta), \quad (13)$$

where

$$Y_0(\omega) := -I^{-1}C(\omega)\omega - I^{-1}D\omega, \\ Y_1(\theta) := \begin{bmatrix} 0 \\ I_y^{-1}k_1h(\theta) \\ 0 \end{bmatrix}, \quad Y_2(\theta) := \begin{bmatrix} -I_x^{-1}s_{\theta_1}k_2h(\theta) \\ 0 \\ I_z^{-1}c_{\theta_1}k_2h(\theta) \end{bmatrix}.$$

Then, it follows from Bullo (2002); Wang et al. (2023) that the closed-loop system (12) can be approximated by the *symmetric product system*

$$\dot{\bar{\theta}} = J(\bar{\theta})\bar{\omega} \quad (14a)$$

$$I\dot{\bar{\omega}} + C(\bar{\omega})\bar{\omega} + D\bar{\omega} = -\frac{I}{4} [\langle Y_1 : Y_1 \rangle(\bar{\theta}) + \langle Y_2 : Y_2 \rangle(\bar{\theta})] \quad (14b)$$

where the *symmetric product* of two vector fields $X, Y : \mathbb{R}^2 \rightarrow \mathbb{R}^3$ corresponding to the system (4) is given by

$$\langle X : Y \rangle(\theta) = \frac{\partial X}{\partial \theta}(\theta)J(\theta)Y(\theta) + \frac{\partial Y}{\partial \theta}(\theta)J(\theta)X(\theta). \quad (15)$$

In (14), the symmetric products $\langle Y_i : Y_i \rangle$ originates from an iterated Lie bracket on the tangent bundle of the configuration manifold. We refer the readers to the proof of (Wang et al., 2023, Theorem 2) for more details. It follows from Bullo (2002); Wang et al. (2023) that the solutions of the closed-loop system (12) in the variables

$$(\tilde{\theta}, \tilde{\omega}) := \left(\theta, \omega - \sum_{i=1}^2 U_i \left(\frac{t}{\varepsilon} \right) Y_i(\theta) \right) \quad (16)$$

approximate the solutions of (14). A direct computation shows that

$$\langle Y_1 : Y_1 \rangle(\theta) = 2k_1^2 I_y^{-2} \frac{\partial h}{\partial \theta_1}(\theta)h(\theta) \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}, \quad (17)$$

$$\langle Y_2 : Y_2 \rangle(\theta) = 2k_2^2 r(\theta_1) \frac{\partial h}{\partial \theta_2}(\theta)h(\theta) \begin{bmatrix} -I_x^{-1}s_{\theta_1} \\ 0 \\ I_z^{-1}c_{\theta_1} \end{bmatrix}, \quad (18)$$

where $r(\theta_1) := I_x^{-1}s_{\theta_1}^2 + I_z^{-1}c_{\theta_1}^2$. Substituting (17)-(18) into (14) yields the *averaged system*

$$\dot{\bar{\theta}} = J(\bar{\theta})\bar{\omega} \quad (19a)$$

$$I\dot{\bar{\omega}} + C(\bar{\omega})\bar{\omega} + D\bar{\omega} = J(\bar{\theta})^\top \Lambda(\bar{\theta}_1) \left[-\frac{1}{2} \frac{\partial h}{\partial \theta}^\top(\bar{\theta})h(\bar{\theta}) \right] \quad (19b)$$

where

$$\Lambda(\bar{\theta}_1) := \begin{bmatrix} k_1^2 I_y^{-1} & 0 \\ 0 & k_2^2 r(\bar{\theta}_1) \end{bmatrix}, \quad (20)$$

and the term in the bracket of (19b) is exactly the negative gradient of the function $\frac{1}{4}h(\bar{\theta})^2$. We conclude that the solutions of the closed-loop system (12) in the variables (16) approximate the solutions of (19).

3.3 Stability Analysis

Next, we provide sufficient conditions for the stability of the averaged system (19). In general, analyzing the

stability of (19) directly using Lyapunov methods is challenging due to the presence of the term $\Lambda(\bar{\theta}_1)$. However, the analysis becomes significantly easier if $\Lambda(\cdot)$ is a constant matrix. Notably, the averaged system (19) is reminiscent of *gradient systems* if $\Lambda(\cdot)$ is a constant matrix. Furthermore, if the function h is quadratic, then the averaged system (19) is reminiscent of a Lagrangian system under PD control, a topic that has been well studied. In fact, one should notice that the matrix $\Lambda(\cdot)$ is uniformly bounded, and the term $r(\bar{\theta}_1)$ satisfies $r(\bar{\theta}_1) \in [I_z^{-1}, I_x^{-1}]$. Hence, in the following, we first analyze the averaged system (19) under the assumption that the matrix $\Lambda(\cdot)$ is constant, *i.e.*, $\Lambda(\cdot) \equiv \bar{\Lambda} := \text{diag}\{\lambda_1, \lambda_2\}$, and provide a strict Lyapunov function for the “frozen dynamics”. Then, we extend the analysis to the case where $\Lambda(\cdot)$ varies, using the time-scale separation method.

First, we show asymptotic stability for the corresponding “frozen dynamics”

$$\dot{\bar{\theta}} = J(\bar{\theta})\bar{\omega} \quad (21a)$$

$$I\dot{\bar{\omega}} + C(\bar{\omega})\bar{\omega} + D\bar{\omega} = J(\bar{\theta})^\top \bar{\Lambda} \left[-\frac{1}{2} \frac{\partial h}{\partial \theta}^\top(\bar{\theta})h(\bar{\theta}) \right], \quad (21b)$$

where $\bar{\Lambda} := \text{diag}\{\lambda_1, \lambda_2\} > 0$. Define the new objective function as

$$\bar{h}(\theta) := \lambda_1 h_1(\theta_1) + \lambda_2 h_2(\theta_2), \quad (22)$$

where functions h_1 and h_2 are given in Assumption 2. Obviously, the functions h and \bar{h} attain their minimum values at the same point θ_* due to the fact that $\lambda_1, \lambda_2 > 0$.

Let us consider the function

$$V_1(\bar{\theta} - \theta_*, \bar{\omega}) := \frac{1}{2}\bar{\omega}^\top I\bar{\omega} + \frac{1}{4}\bar{h}(\bar{\theta})^2 - \frac{1}{4}\bar{h}(\theta_*)^2. \quad (23)$$

It is clear that the function V_1 is position definite. Taking the total derivative along trajectories of (21) yields

$$\begin{aligned} \dot{V}_1 &= \bar{\omega}^\top \left[-C(\bar{\omega})\bar{\omega} - D\bar{\omega} + J(\bar{\theta})^\top \bar{\Lambda} \left(-\frac{1}{2} \frac{\partial h}{\partial \theta}^\top(\bar{\theta})h(\bar{\theta}) \right) \right] \\ &\quad + \frac{1}{2}\bar{h}(\bar{\theta}) \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta})J(\bar{\theta})\bar{\omega} \\ &= -\bar{\omega}^\top D\bar{\omega} \leq 0, \end{aligned} \quad (24)$$

where we use the property that the matrix $C(\cdot)$ is skew-symmetric and the fact that $\frac{\partial \bar{h}}{\partial \theta}(\theta) = \bar{\Lambda} \frac{\partial h}{\partial \theta}(\theta)$ everywhere. Thus, we conclude that V_1 is a weak Lyapunov function for the system (21), and asymptotic stability of the equilibrium point $(\bar{\theta}, \bar{\omega}) = (\theta_*, 0)$ comes from verifying the LaSalle’s condition on the set $\{\dot{V}_1 = 0\}$. If the function h is radially unbounded, we conclude that the equilibrium point $(\bar{\theta}, \bar{\omega}) = (\theta_*, 0)$ is globally asymptotically stable.

To proceed with the Lyapunov analysis for the averaged system (19), we need a *strict* Lyapunov function for (21). Define $d_m := \min\{d_x, d_y, d_z\}$, $d_M := \max\{d_x, d_y, d_z\}$, $I_m := \min\{I_x, I_y, I_z\}$, and $I_M := \max\{I_x, I_y, I_z\}$. Let us consider the function

$$V_2(\bar{\theta}, \bar{\omega}) := \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta})J(\bar{\theta})I\bar{\omega}, \quad (25)$$

where its total derivative along trajectories of (21) is

$$\begin{aligned}
\dot{V}_2 &= \bar{\omega}^\top J(\bar{\theta})^\top \frac{\partial^2 \bar{h}}{\partial \theta^2}(\bar{\theta}) J(\bar{\theta}) I \bar{\omega} + \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta}) J(\bar{\theta}) I \bar{\omega} \\
&\quad - \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta}) J(\bar{\theta}) \left[C(\bar{\omega}) \bar{\omega} + D \bar{\omega} + \frac{h(\bar{\theta})}{2} J(\bar{\theta})^\top \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta}) \right] \\
&\leq -\frac{1}{2} h(\theta_*) \left| \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta}) \right|^2 + 6 \bar{h}_M I_M |\bar{\omega}|^2 \\
&\quad + \sqrt{6} [I_M |\bar{\omega}| + 3 I_M |\bar{\omega}| + d_M] \left| \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta}) \right| |\bar{\omega}|, \quad (26)
\end{aligned}$$

where we use the facts that $\|J(\cdot)\| \leq \sqrt{6}$, $J(\cdot)J(\cdot)^\top = I_{2 \times 2}$, $\|J(\bar{\theta})\| \leq \sqrt{6}|\bar{\omega}|$, $\|C(\omega)\| \leq 3I_M|\omega|$, $\|\frac{\partial^2 \bar{h}}{\partial \theta^2}(\cdot)\| \leq \bar{h}_M$, and $h(\theta) \geq h(\theta_*)$ everywhere.

Note that $|\bar{\omega}| \leq \sqrt{\frac{2}{I_m}} \sqrt{V_1}$. Defining the function $P_1 : \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}_{\geq 0}$ as

$$P_1(l) := \sqrt{6}d_M + 8\sqrt{3}l \frac{I_M}{\sqrt{I_m}}, \quad (27)$$

we have

$$\dot{V}_2 \leq -\frac{1}{2} h(\theta_*) \left| \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta}) \right|^2 + 6 \bar{h}_M I_M |\bar{\omega}|^2 + P_1(V_1) \left| \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta}) \right| |\bar{\omega}|.$$

It follows from Young's Inequality that

$$P_1(V_1) \left| \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta}) \right| |\bar{\omega}| \leq \frac{h(\theta_*)}{4} \left| \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta}) \right|^2 + \frac{1}{h(\theta_*)} P_1(V_1)^2 |\bar{\omega}|^2.$$

Defining the function $P_2 : \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}_{\geq 0}$ as

$$P_2(l) := 6 \bar{h}_M I_M + \frac{1}{h(\theta_*)} P_1(l)^2 \quad (28)$$

yields

$$\dot{V}_2 \leq -\frac{1}{4} h(\theta_*) \left| \frac{\partial \bar{h}}{\partial \theta}(\bar{\theta}) \right|^2 + P_2(V_1) |\bar{\omega}|^2. \quad (29)$$

Finally, define the function $P_3 : \mathbb{R}_{\geq 0} \rightarrow \mathbb{R}_{\geq 0}$ as

$$P_3(l) := \frac{1}{d_m} \int_0^l P_2(m) dm + P_0 l, \quad (30)$$

where

$$P_0 := \max \left\{ \frac{12 I_M^2}{I_m}, \frac{4 \bar{h}_M^2}{h(\theta_*)} \lambda_{\min}^{-1} \left[\frac{\partial^2 \bar{h}}{\partial \theta^2}(\theta_*) \right] \right\}. \quad (31)$$

We have the following result.

Proposition 2. Let λ_m, λ_M be two positive real numbers satisfying $\lambda_m < \lambda_M$. For each $\lambda := (\lambda_1, \lambda_2) \in [\lambda_m, \lambda_M] \times [\lambda_m, \lambda_M]$, the equilibrium point of the system (21) $(\bar{\theta}, \bar{\omega}) = (\theta_*, 0)$ is asymptotically stable. Furthermore, if the function h is radially unbounded, then the equilibrium point $(\bar{\theta}, \bar{\omega}) = (\theta_*, 0)$ is globally asymptotically stable. Moreover, the function $V_\lambda : \mathbb{R}^2 \times \mathbb{R}^3 \rightarrow \mathbb{R}_{\geq 0}$ defined as

$$V_\lambda(\bar{\theta} - \theta_*, \bar{\omega}) := V_2(\bar{\theta}, \bar{\omega}) + P_3(V_1(\bar{\theta} - \theta_*, \bar{\omega})) \quad (32)$$

is a strict Lyapunov function for the system (21).

The proof of Proposition 2 is based on Lyapunov's direct method. The complete proof can be found in Wang et al. (2025).

Next, we use the strict Lyapunov function V_λ for the frozen dynamics to analyze the full dynamics (19). First, noting that $r(\theta_1) := I_x^{-1} s_{\theta_1}^2 + I_z^{-1} c_{\theta_1}^2$ is bounded uniformly in its initial conditions, i.e., $r(\bar{\theta}_1) \in [I_z^{-1}, I_x^{-1}]$, let us substitute the solution $\bar{\theta}_1(t)$ of (19) into $r(\theta_1)$ and denote $\bar{r}(t) := r(\bar{\theta}_1(t))$. Then, $\dot{r}(t) = (I_x^{-1} - I_z^{-1}) \sin(2\bar{\theta}_1(t)) \dot{\bar{\theta}}_1(t)$ is locally

Lipschitz due to the fact that the system (19) is smooth and following Gronwall's inequality. Consequently, $\dot{r}(t)$ is also bounded. With a slight abuse of notation, defining $\lambda_1 := k_1^2 I_y^{-1}$, $\lambda_2(t) := k_2^2 \bar{r}(t)$, and $\bar{\Lambda}(t) := \text{diag}\{\lambda_1, \lambda_2(t)\}$, we rewrite the averaged system (19) as

$$\dot{\bar{\theta}} = J(\bar{\theta}) \bar{\omega} \quad (33a)$$

$$I \dot{\bar{\omega}} + C(\bar{\omega}) \bar{\omega} + D \bar{\omega} = J(\bar{\theta})^\top \bar{\Lambda}(t) \left[-\frac{1}{2} \frac{\partial h}{\partial \theta}(\bar{\theta}) h(\bar{\theta}) \right] \quad (33b)$$

and consider (33) as a *slowly time-varying system* with the slowly varying parameter λ_2 because $\dot{r}(t)$ is bounded and k_2 can be chosen arbitrarily small in $\lambda_2(t) = k_2^2 \bar{r}(t)$. Now, let us consider the Lyapunov function candidate V_λ and calculate its total derivative along trajectories of (33), which yields

$$\dot{V}_\lambda|_{(33)} = \dot{V}_\lambda|_{(21)} + \frac{\partial V_\lambda}{\partial \lambda_2} \dot{\lambda}_2(t). \quad (34)$$

Note that in (34), $\dot{V}_\lambda|_{(21)}$ is negative definite with respect to $(\bar{\theta} - \theta_*, \bar{\omega})$. Moreover, $\dot{\lambda}_2(t)$ can be made arbitrarily small by choosing a sufficiently small control parameter k_2 .

Proposition 3. Consider the system (33) and its equilibrium point $(\bar{\theta}, \bar{\omega}) = (\theta_*, 0)$. Assume that $k_1 > 0$. Then, there exists a positive constant $\bar{k}_2 > 0$ such that for all $k_2 \in (0, \bar{k}_2]$, the equilibrium point $(\bar{\theta}, \bar{\omega}) = (\theta_*, 0)$ is uniformly asymptotically stable.

The proof of Proposition 3 can be found in Wang et al. (2025).

Finally, we can state the following consequence of Propositions 1 and 3, which is our main result.

Proposition 4. Consider the Euler-Lagrangian system (4) with the control law (11). Suppose that the objective function h satisfies Assumptions 1-3. Then, there exists $\varepsilon_0 > 0$ such that for every $\varepsilon \in (0, \varepsilon_0]$ and every $k_1 > 0$, there exists $\bar{k}_2 > 0$ such that for all $k_2 \in (0, \bar{k}_2]$, the equilibrium point of the closed-loop system (12) $(\theta, \omega) = (\theta_*, 0)$ is locally practically uniformly asymptotically stable in the variables of (16).

4. SIMULATION RESULTS

As an example, we consider the antenna system (4) with an antenna panel of dimensions: length = 0.6 m, width = 0.3 m, and height = 0.1 m. The mass of the antenna panel is 10 kg. By calculation, the moments of inertia are determined as $I_x = 0.0833$, $I_y = 0.3083$, and $I_z = 0.15$. The damping coefficients are given by $d_x = 0.1$, $d_y = 0.1$, and $d_z = 0.1$. All parameters are given in SI units. Three initial postures of the antenna are randomly generated as $\theta_{\text{blue}}(0) = [-0.3849, -0.7422]^\top$, $\theta_{\text{red}}(0) = [1.9775, 0.7854]^\top$, and $\theta_{\text{yellow}}(0) = [-0.4916, 2.6121]^\top$. All initial angular velocities are assumed to be zero.

In the simulations, we assume that the unknown cost function to be optimized is given by $h(\theta) := \frac{1}{2}(\theta_1 - \theta_{1d})^2 + \frac{1}{2}(\theta_2 - \theta_{2d})^2 + 0.2$, where $(\theta_{1d}, \theta_{2d}) = (\frac{\pi}{4}, \frac{\pi}{2})$. We choose the input dither signals as $u_1(t) := \cos(t)$ and $u_2(t) := \sin(t)$. The control parameters are set to $\varepsilon = 0.01$, $k_1 = 0.2$, and

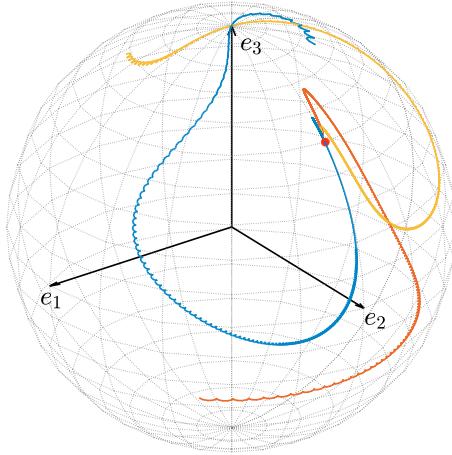


Fig. 2. Paths of the attitude of the closed-loop antenna system on \mathbb{S}^2 , where (e_1, e_2, e_3) denotes the standard basis for \mathbb{R}^3 . The red dot in the figure represents the desired posture, where the function h attains its minimum value at the point.

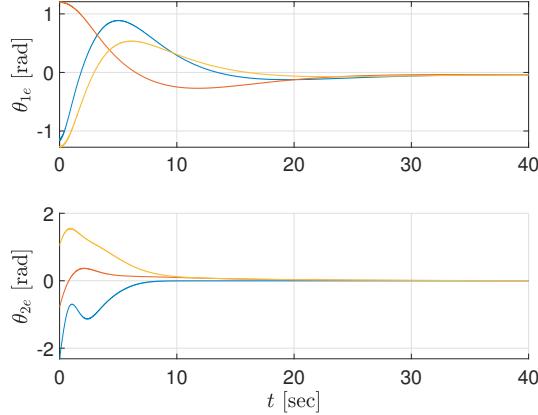


Fig. 3. Error trajectories of the antenna pointing system.

$k_2 = 0.1$. The tracking errors are defined as $\theta_{1e} := \theta_1 - \theta_{1d}$ and $\theta_{2e} := \theta_2 - \theta_{2d}$.

The simulation results are presented in Figs. 2–3. Figure 2 illustrates the three paths of the antenna system's attitude under the extremum-seeking controller. The red dot in the figure represents the desired posture $(\theta_{1d}, \theta_{2d})$, where the function h attains its minimum value. The figure shows that the antenna's posture converges to the desired position in all three simulations. Figure 3 displays the error trajectories of the closed-loop antenna pointing system, demonstrating that the tracking errors converge to a small neighborhood around the origin in all three simulations. These simulation results indicate that, although Proposition 4 asserts local practical uniform asymptotic stability, the domain of attraction may not necessarily be small.

5. CONCLUSION

In this paper, we study the extremum seeking control problem for a two-degree-of-freedom antenna pointing system, assuming that only real-time signal measurements are available. The reference (desired) attitude of the antenna is supposed to be unknown. Utilizing the symmetric product

approximation, we propose an extremum seeking control strategy that enables the antenna to adjust its direction to maximize the received signal strength autonomously. Our theoretical analysis demonstrates local practical uniform asymptotic stability for the closed-loop system. Numerical simulations further illustrate the effectiveness of our approach.

REFERENCES

Ariyur, K.B. and Krstić, M. (2003). *Real-time optimization by extremum-seeking control*. John Wiley & Sons, Hoboken, NJ.

Bullo, F. (2002). Averaging and vibrational control of mechanical systems. *SIAM J. Control Optim.*, 41(2), 542–562.

Bullo, F. and Lewis, A.D. (2005). *Geometric Control of Mechanical Systems*, volume 49. Springer, New York, NY.

Dürr, H.B., Krstić, M., Scheinker, A., and Ebenbauer, C. (2017). Extremum seeking for dynamic maps using lie brackets and singular perturbations. *Automatica*, 83, 91–99.

Dürr, H.B., Stanković, M.S., Ebenbauer, C., and Johansson, K.H. (2013). Lie bracket approximation of extremum seeking systems. *Automatica*, 49(6), 1538–1552.

Gawronski, W. (2001). Antenna control systems: from PI to H_∞ . *IEEE Antennas and Propagation Magazine*, 43(1), 52–60.

Gawronski, W. (2007). Control and pointing challenges of large antennas and telescopes. *IEEE Trans. Control Syst. Technol.*, 15(2), 276–289.

Moreau, L. and Aeyels, D. (2000). Practical stability and stabilization. *IEEE Trans. Autom. Contr.*, 45(8), 1554–1558.

Mulla, A.A. and Vasambekar, P.N. (2016). Overview on the development and applications of antenna control systems. *Annu. Rev. Control*, 41, 47–57.

Scheinker, A. (2024). 100 years of extremum seeking: A survey. *Automatica*, 161, 111481.

Scheinker, A. and Krstić, M. (2017). *Model-free stabilization by extremum seeking*. Springer, Cham, Switzerland.

Shore, S., Lane, S., and Danielson, C. (2024). Extremum seeking control techniques for antenna pointing. In *Proc. Amer. Contr. Conf.*, 5082–5087. IEEE.

Suttner, R. (2019). Extremum seeking control for an acceleration controlled unicycle. *IFAC-PapersOnLine*, 52(16), 676–681.

Suttner, R. (2022). Extremum-seeking control for a class of mechanical systems. *IEEE Trans. Autom. Contr.*, 68(2), 1200–1207.

Suttner, R. and Krstić, M. (2023). Extremum seeking control for fully actuated mechanical systems on lie groups in the absence of dissipation. *Automatica*, 152, 110945.

Wang, B., Ashrafiou, H., and Nersesov, S.G. (2025). Extremum seeking control for antenna pointing via symmetric product approximation. *arXiv preprint*, arXiv:2502.17252. URL <https://arxiv.org/abs/2502.17252>.

Wang, B., Nersesov, S., Ashrafiou, H., Naseradinmousavi, P., and Krstić, M. (2023). Underactuated source seeking by surge force tuning: Theory and boat experiments. *IEEE Trans. Control Syst. Technol.*, 31(4), 1649–1662.